

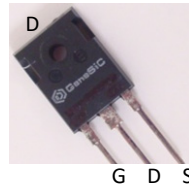
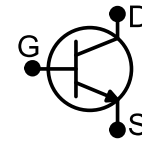
## Normally – OFF Silicon Carbide Junction Transistor

$V_{DS}$	=	1700 V
$R_{DS(ON)}$	=	1.5 $\Omega$
$I_D$ (@ 25°C)	=	2 A
$h_{FE}$ (@ 25°C)	=	100

### Features

- 175 °C Maximum Operating Temperature
- Gate Oxide Free SiC Switch
- Exceptional Safe Operating Area
- Excellent Gain Linearity
- Temperature Independent Switching Performance
- Low Output Capacitance
- Positive Temperature Coefficient of  $R_{DS,ON}$
- Suitable for Connecting an Anti-parallel Diode

### Package


**TO-247**


### Advantages

- Compatible with Si MOSFET/IGBT Gate Drive ICs
- > 20  $\mu$ s Short-Circuit Withstand Capability
- Lowest-in-class Conduction Losses
- High Circuit Efficiency
- Minimal Input Signal Distortion
- High Amplifier Bandwidth

### Applications

- Down Hole Oil Drilling, Geothermal Instrumentation
- Hybrid Electric Vehicles (HEV)
- Solar Inverters
- Switched-Mode Power Supply (SMPS)
- Power Factor Correction (PFC)
- Induction Heating
- Uninterruptible Power Supply (UPS)
- Motor Drives

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### Section I: Absolute Maximum Ratings

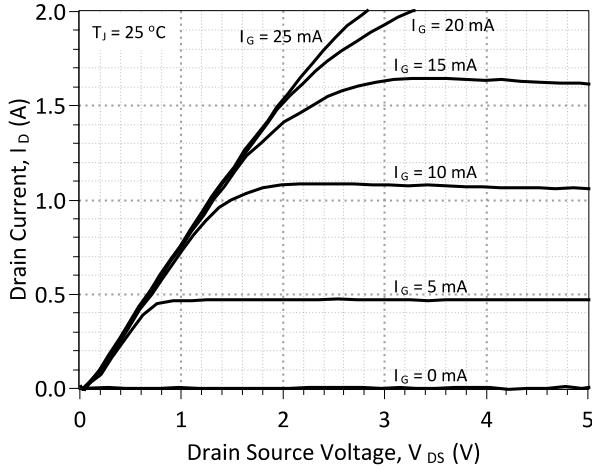
Parameter	Symbol	Conditions	Value	Unit	Notes
Drain – Source Voltage	$V_{DS}$	$V_{GS} = 0$ V	1700	V	
Continuous Drain Current	$I_D$	$T_C = 25^\circ\text{C}$	2	A	
Continuous Gate Current	$I_G$		0.1	A	
Turn-Off Safe Operating Area	RBSOA	$T_{VJ} = 175^\circ\text{C}$ , Clamped Inductive Load	$I_{D,max} = 2$ @ $V_{DS} \leq V_{DSmax}$	A	Fig. 9
Short Circuit Safe Operating Area	SCSOA	$T_{VJ} = 175^\circ\text{C}$ , $I_G = 0.2$ A, $V_{DS} = 1200$ V, Non Repetitive	> 20	$\mu$ s	
Reverse Gate – Source Voltage	$V_{SG}$		30	V	
Reverse Drain – Source Voltage	$V_{SD}$		25	V	
Storage Temperature	$T_{stg}$		-55 to 175	$^\circ\text{C}$	

**Section II: Static Electrical Characteristics**

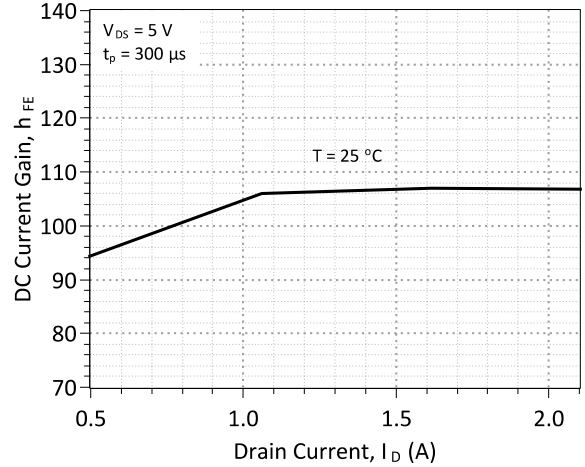
Parameter	Symbol	Conditions	Value			Unit	Notes
			Min.	Typical	Max.		
<b>A: On State</b>							
Drain – Source On Resistance	$R_{DS(ON)}$	$I_D = 1\text{ A}, T_J = 25\text{ }^\circ\text{C}$		1.5		$\Omega$	
Gate – Source Saturation Voltage	$V_{GS,SAT}$	$I_D = 1\text{ A}, I_D/I_G = 40, T_J = 25\text{ }^\circ\text{C}$ $I_D = 1\text{ A}, I_D/I_G = 30, T_J = 175\text{ }^\circ\text{C}$		3.45 3.22		V	Fig. 4
DC Current Gain	$h_{FE}$	$V_{DS} = 5\text{ V}, I_D = 1\text{ A}, T_J = 25\text{ }^\circ\text{C}$		100		–	Fig. 2
<b>B: Off State</b>							
Drain Leakage Current	$I_{DSS}$	$V_{DS} = 1700\text{ V}, V_{GS} = 0\text{ V}, T_J = 25\text{ }^\circ\text{C}$		0.03		$\mu\text{A}$	Fig. 5
Gate Leakage Current	$I_{SG}$	$V_{SG} = 20\text{ V}, T_J = 25\text{ }^\circ\text{C}$		20		nA	
<b>C: Thermal</b>							
Thermal resistance, junction - case	$R_{thJC}$			4.83		$^\circ\text{C/W}$	Fig. 7

**Section III: Figures**

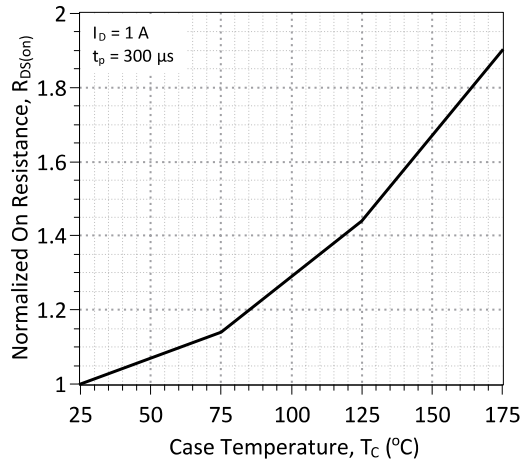
**A: Static Characteristics**



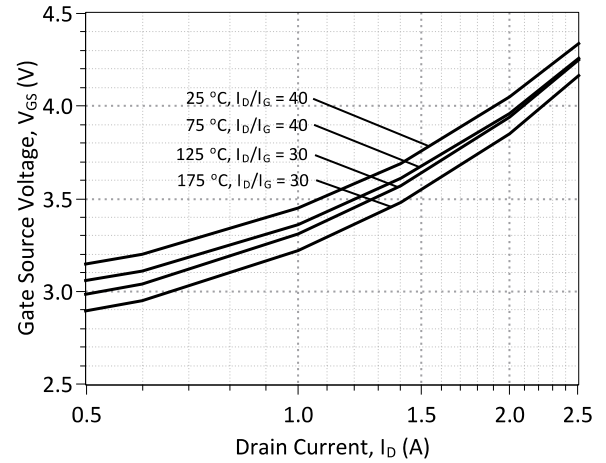
**Figure 1: Typical Output Characteristics at 25 °C**



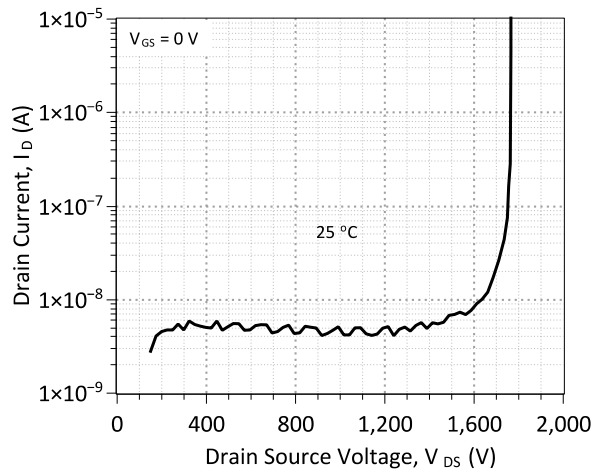
**Figure 2: DC Current Gain vs. Drain Current**



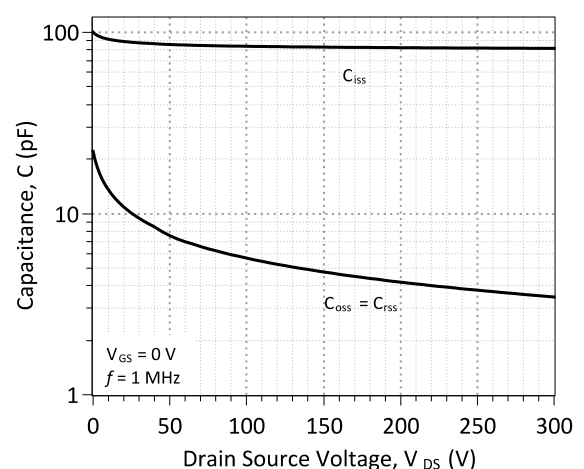
**Figure 3: On-Resistance vs. Temperature**



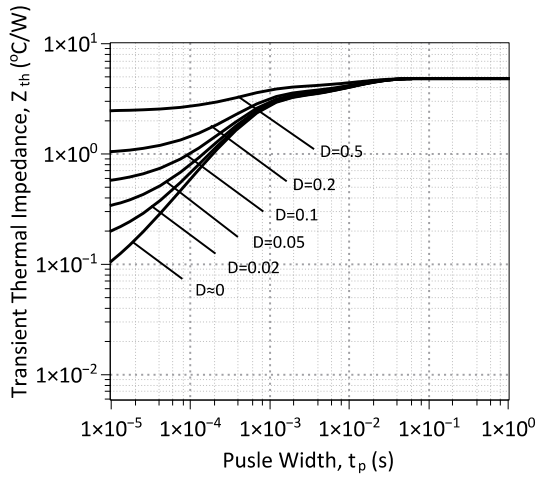
**Figure 4: Typical Gate – Source Saturation Voltage**



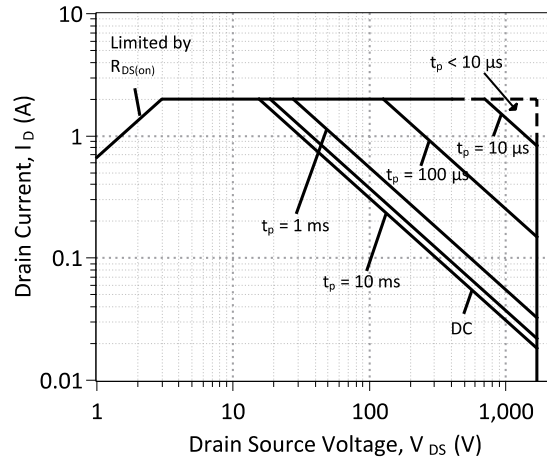
**Figure 5: Typical Blocking Characteristics**



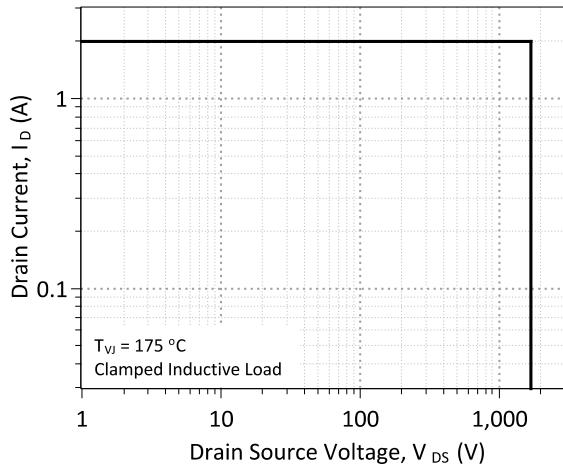
**Figure 6: Input, Output, and Reverse Transfer Capacitance**



**Figure 7: Transient Thermal Impedance**



**Figure 8: Forward Bias Safe Operating Area at  $T_c = 25^\circ\text{C}$**



**Figure 9: Turn-Off Safe Operating Area**

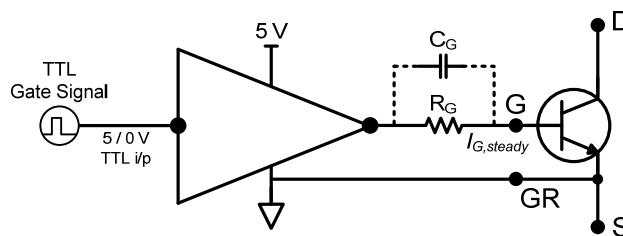
**Section IV: Driving the GR1500JT17-247**

Drive Topology	Gate Drive Power Consumption	Switching Frequency	Application Emphasis
TTL Logic	High	Low	Wide Temperature Range
Constant Current	Medium	Medium	Wide Temperature Range
High Speed – Boost Capacitor	Medium	High	Fast Switching
High Speed – Boost Inductor	Low	High	Ultra Fast Switching
Proportional	Lowest	High	Wide Drain Current Range
Pulsed Power	Medium	N/A	Pulse Power

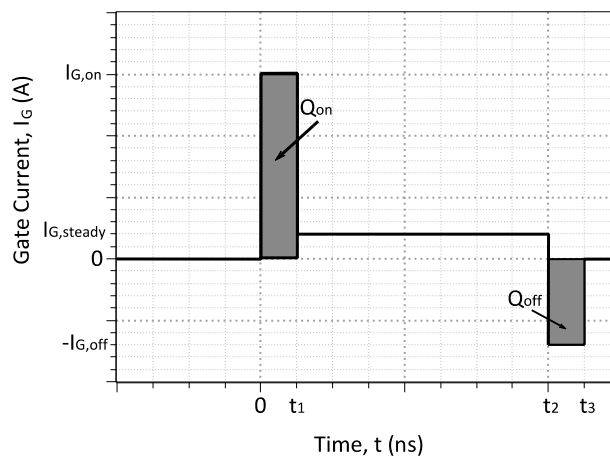
**Static TTL Logic Driving**

The GR1500JT17-247 may be driven with direct (5 V) TTL logic and current amplification. The amplified current level of the supply must meet or exceed the steady state gate current ( $I_{G,steady}$ ) required to operate the GR1500JT17-247. Minimum  $I_{G,steady}$  is dependent on the anticipated drain current  $I_D$  through the SJT and the DC current gain  $h_{FE}$ , it may be calculated from the following equation. An accurate value of the  $h_{FE}$  may be read from Figure 2. An optional resistor  $R_G$  may be used in series with the gate pin to trim  $I_{G,steady}$ , also an optional capacitor  $C_G$  may be added in parallel with  $R_G$  to facilitate faster SJT switching if desired, further details on these options are given in the following section.

$$I_{G,steady} \approx \frac{I_D}{h_{FE}(T, I_D)} * 1.5$$


**Figure 10: TTL Gate Drive Schematic**
**High Speed Driving**

The SJT is a current controlled transistor which requires a positive gate current for turn-on and to remain in on-state. An idealized gate current waveform for ultra-fast switching of the SJT while maintaining low gate drive losses is shown in Figure 11, it features a positive current peak during turn-on, a negative current peak during turn-off, and continuous gate current during on-state.


**Figure 11: An idealized gate current waveform for fast switching of an SJT.**

An SJT is rapidly switched from its blocking state to on-state when the necessary gate charge,  $Q_G$ , for turn-on is supplied by a burst of high gate current,  $I_{G,on}$ , until the SJT gate-source capacitance,  $C_{GS}$ , and gate-drain capacitance,  $C_{GD}$ , are fully charged.

$$Q_{on} = I_{G,on} * t_1$$

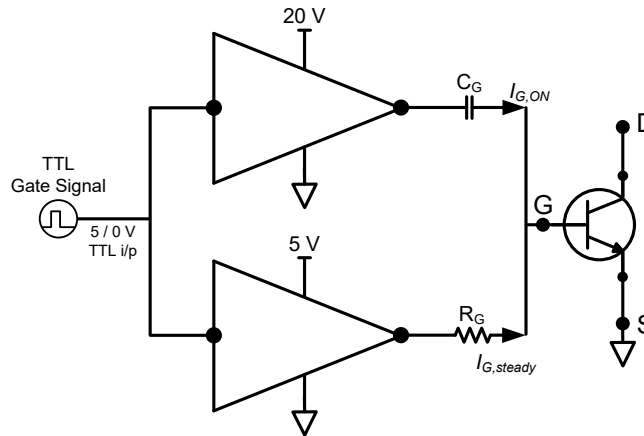
$$Q_{on} \geq Q_{gs} + Q_{gd}$$

Ideally,  $I_{G,on}$  should terminate when the drain voltage falls to its on-state value in order to avoid unnecessary drive losses during the steady on-state. In practice, the rise time of the  $I_{G,on}$  pulse is affected by the parasitic inductances,  $L_{par}$  in the device package and drive circuit. A voltage developed across the parasitic inductance in the source path,  $L_s$ , can de-bias the gate-source junction, when high drain currents begin to flow through the device. The voltage applied to the gate pin should be maintained high enough, above the  $V_{GS,sat}$  (see Figure 7) level to counter these effects.

A high negative peak current,  $-I_{G,off}$  is recommended at the start of the turn-off transition, in order to rapidly sweep out the injected carriers from the gate, and achieve rapid turn-off. Turn off can be achieved with  $V_{GS} = 0$  V, however a negative gate voltage  $V_{GS}$  may be used in order to speed up the turn-off transition.

**A:1: High Speed, Low Loss Drive with Boost Capacitor**

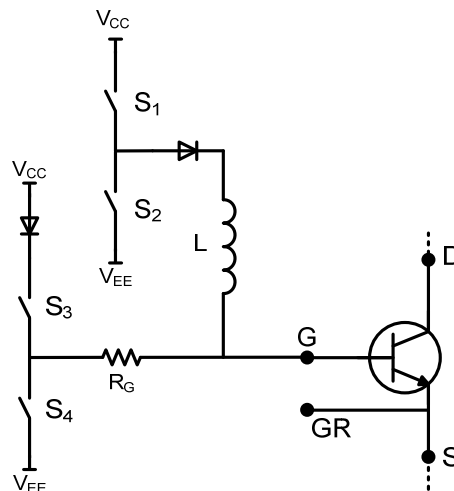
The GR1500JT17-247 may be driven using a High Speed, Low Loss Drive with Boost Capacitor topology in which multiple voltage levels, a gate resistor, and a gate capacitor are used to provide fast switching current peaks at turn-on and turn-off and a continuous gate current while in on-state. An example of this topology is shown in Figure 12.



**Figure 12: Simplified Boost Capacitor Drive Topology.**

**A:2: High Speed, Low Loss Drive with Boost Inductor**

A High Speed, Low-Loss Driver with Boost Inductor is also capable of driving the GR1500JT17-247 at high-speed. It utilizes a gate drive inductor instead of a capacitor to provide the high-current gate current pulses  $I_{G,on}$  and  $I_{G,off}$ . During operation, inductor  $L$  is charged to a specified  $I_{G,on}$  current value then made to discharge  $I_L$  into the S-JT gate pin using logic control of  $S_1$ ,  $S_2$ ,  $S_3$ , and  $S_4$ , as shown in Figure 13. After turn on, while the device remains on the necessary steady state gate current  $I_{G,steady}$  is supplied from source  $V_{CC}$  through  $R_G$ . Please refer to the article “A current-source concept for fast and efficient driving of silicon carbide transistors” by Dr. Jacek Rąbkowski for additional information on this driving topology.<sup>3</sup>



**Figure 13: Simplified Inductive Pulsed Drive Topology**

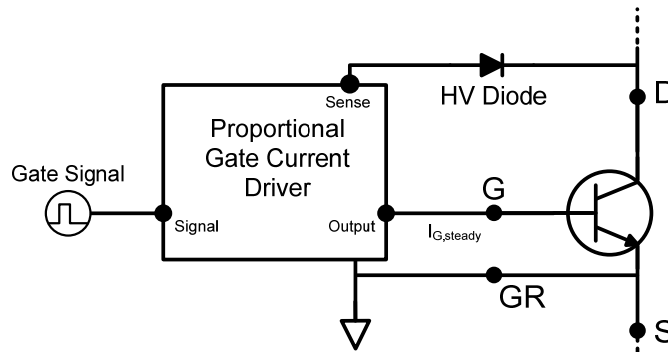
<sup>3</sup> – Archives of Electrical Engineering. Volume 62, Issue 2, Pages 333–343, ISSN (Print) 0004-0746, DOI: 10.2478/ae-2013-0026, June 2013

**B: Proportional Gate Current Driving**

For applications in which the GR1500JT17-247 will operate over a wide range of drain current conditions, it may be beneficial to drive the device using a proportional gate drive topology to optimize gate drive power consumption. A proportional gate driver relies on instantaneous drain current  $I_D$  feedback to vary the steady state gate current  $I_{G,steady}$  supplied to the GR1500JT17-247

**Voltage Controlled Proportional Driver**

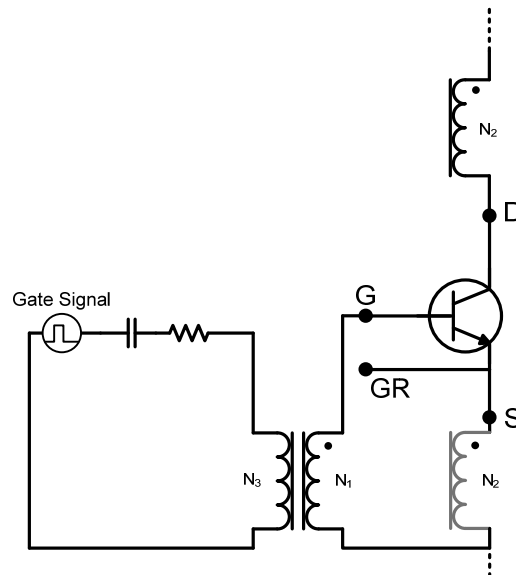
The voltage controlled proportional driver relies on a gate drive IC to detect the GR1500JT17-247 drain-source voltage  $V_{DS}$  during on-state to sense  $I_D$ . The gate drive IC will then increase or decrease  $I_{G,steady}$  in response to  $I_D$ . This allows  $I_{G,steady}$ , and thus the gate drive power consumption, to be reduced while  $I_D$  is relatively low or for  $I_{G,steady}$  to increase when is  $I_D$  higher. A high voltage diode connected between the drain and sense protects the IC from high-voltage when the driver and GR1500JT17-247 are in off-state. A simplified version of this topology is shown in Figure 14, additional information will be available in the future at <http://www.genesicsemi.com/commercial-sic/sic-junction-transistors/>



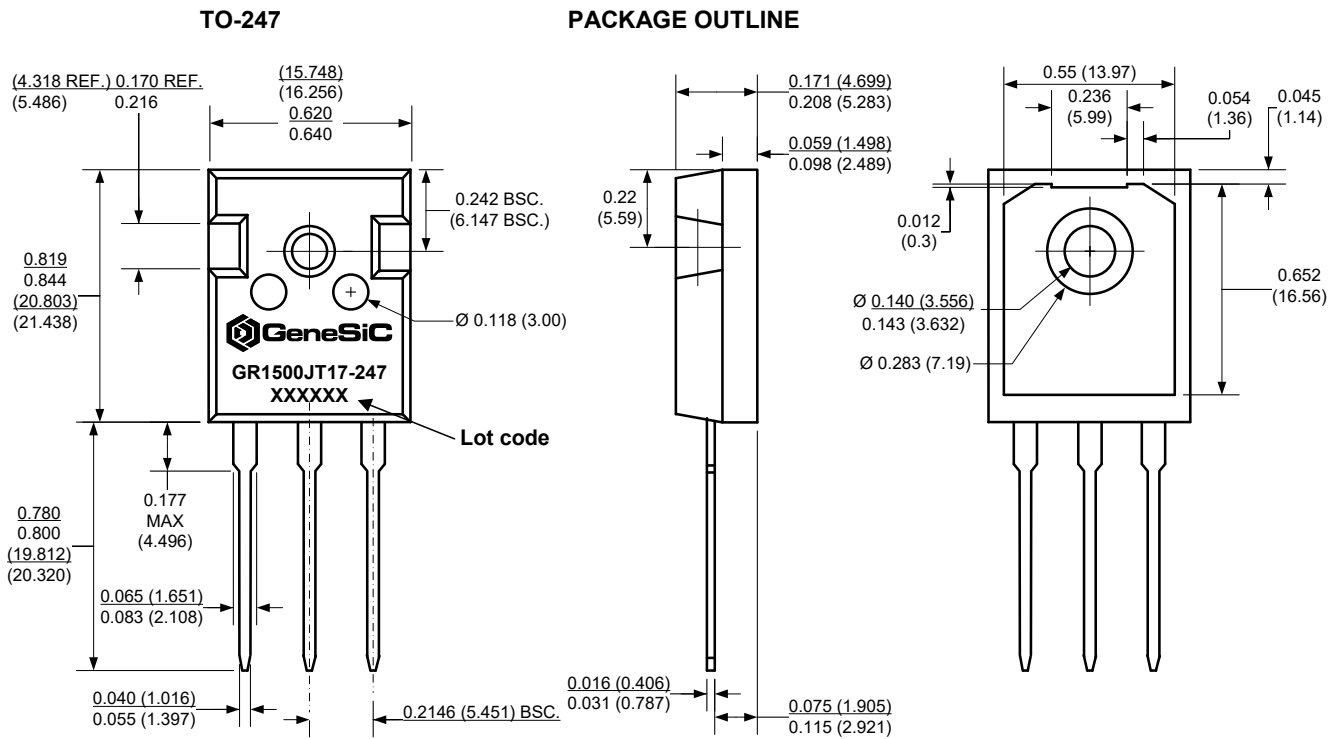
**Figure 14: Simplified Voltage Controlled Proportional Driver**

**Current Controlled Proportional Driver**

The current controlled proportional driver relies on a low-loss transformer in the drain or source path to provide feedback  $I_D$  of the GR1500JT17-247 during on-state to supply  $I_{G,steady}$  into the device gate.  $I_{G,steady}$  will then increase or decrease in response to  $I_D$  at a fixed forced current gain which is set by the turns ratio of the transformer,  $h_{force} = I_D / I_G = N_2 / N_1$ . GR1500JT17-247 is initially turned-on using a gate current pulse supplied into an RC drive circuit to allow  $I_D$  current to begin flowing. This topology allows  $I_{G,steady}$ , and thus the gate drive power consumption, to be reduced while  $I_D$  is relatively low or for  $I_{G,steady}$  to increase when is  $I_D$  higher. A simplified version of this topology is shown in Figure 15, additional information will be available in the future at <http://www.genesicsemi.com/commercial-sic/sic-junction-transistors/>.



**Figure 15: Simplified Current Controlled Proportional Driver**

**Section V: Package Dimensions**


- NOTE**
1. CONTROLLED DIMENSION IS INCH. DIMENSION IN BRACKET IS MILLIMETER.
  2. DIMENSIONS DO NOT INCLUDE END FLASH, MOLD FLASH, MATERIAL PROTRUSIONS

Revision History			
Date	Revision	Comments	Supersedes
2016/04/04	0	Initial release	

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**Section VI: SPICE Model Parameters**

This is a secure document. Please copy this code from the SPICE model PDF file on our website ([http://www.genesicsemi.com/images/products\\_sic/sjt/GR1500JT17-247\\_SPICE.pdf](http://www.genesicsemi.com/images/products_sic/sjt/GR1500JT17-247_SPICE.pdf)) into LTSPICE (version 4) software for simulation of the GR1500JT17-247.

```
*      MODEL OF GeneSiC Semiconductor Inc.
*
*      $Revision:   1.0           $
*      $Date:      04-APR-2016   $
*
*      GeneSiC Semiconductor Inc.
*      43670 Trade Center Place Ste. 155
*      Dulles, VA 20166
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*      OF ANY KIND EITHER EXPRESSED OR IMPLIED, INCLUDING BUT NOT LIMITED
*      TO ANY IMPLIED WARRANTIES OF MERCHANTABILITY AND FITNESS FOR A
*      PARTICULAR PURPOSE."
*      Models accurate up to 2 times rated drain current.
*
.model GR1500JT12 NPN
+ IS      9.8338E-48
+ ISE     1.0733E-26
+ EG      3.23
+ BF      110
+ BR      0.55
+ IKF     5000
+ NF      1
+ NE      2
+ RB      20
+ IRB     0.002
+ RBM     0.6
+ RE      0.003
+ RC      1.5
+ CJC     25E-12
+ VJC     3
+ MJC     0.5
+ CJE     80E-12
+ VJE     3
+ MJE     0.5
+ XTI     3
+ XTB     -1.5
+ TRC1    6.5E-3
+ VCEO    1700
+ MFG     GeneSiC_Semiconductor
*
*      End of GR1500JT12 SPICE Model
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